

# Bouncing, rolling and sticking of stiff and soft bodies

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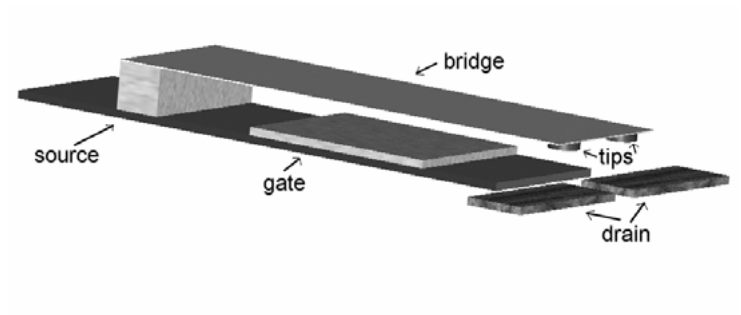
Dipartimento di Ingegneria delle Strutture, delle Acque e del Terreno  
Università dell'Aquila - Italy

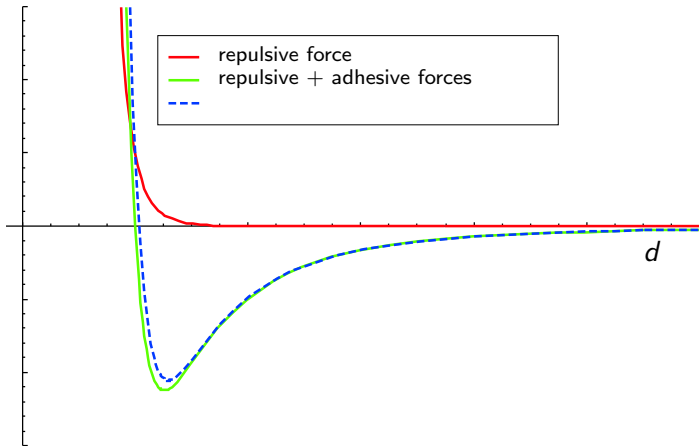
INTAS Project:  
*Some Nonclassical Problems For Thin Structures,*  
Rome, 22-23 Jan 2008

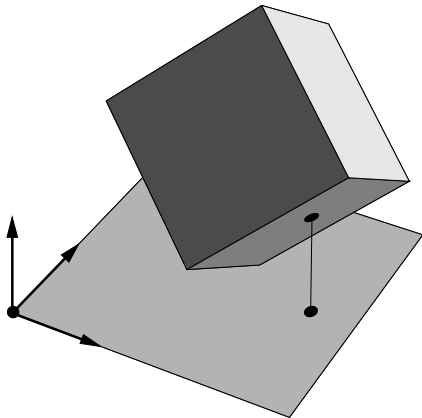
*Based on a joint work with:*  
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# Micro switch







## Rigid body

A motion of the body  $\mathcal{B}$  is described at each time  $t$  by a placement defined on the *paragon shape*  $\mathcal{D}$  :

$$p : \mathcal{D} \times \mathcal{J} \rightarrow \mathcal{E}$$

characterized by the following representation:

$$p(x, t) = p_o(t) + R(t)(x - x_o)$$

where  $R(t) : \mathcal{V} \rightarrow \mathcal{V}$  is a rotation in the translation space of  $\mathcal{E}$ .

Test velocity fields:

$$w(x) = w_o + WR(t)(x - x_o),$$

with  $\text{sym } W = 0$

## Affine body

A motion of the body  $\mathcal{B}$  is described at each time  $t$  by a placement defined on the *paragon shape*  $\mathcal{D}$  :

$$p : \mathcal{D} \times \mathcal{J} \rightarrow \mathcal{E}$$

characterized by the following representation:

$$p(x, t) = p_o(t) + F(t)(x - x_o)$$

where  $F(t) : \mathcal{V} \rightarrow \mathcal{V}$  is linear and such that  $\det F(t) > 0$

Test velocity fields:

$$w(x) = w_o + GF(t)(x - x_o)$$

# Rigid body

Balance principle:

$$\int_{\mathcal{D}} b \cdot w \, dV + \int_{\partial\mathcal{D}} q \cdot w \, dA = 0 \quad \forall w, \forall t$$

Equations of motion:

$$-m \ddot{p}_o(t) - m g + f(t) = 0$$

$$\text{skw}(-\ddot{R}(t) J R(t)^T + M(t) R(t)^T) = 0$$



# Affine body

Balance principle:

$$-S \cdot GF \operatorname{vol} \mathcal{D} + \int_{\mathcal{D}} b \cdot w \, dV + \int_{\partial \mathcal{D}} q \cdot w \, dA = 0 \quad \forall w, \forall t$$

Equations of motion:

$$-m \ddot{p}_o(t) - m g + f(t) = 0$$

$$-\ddot{F}(t) J F(t)^T + (M(t) - S(t) \operatorname{vol} \mathcal{D}) F(t)^T = 0$$

Mass and Euler tensor:

$$m := \int_{\mathcal{D}} \rho dV;$$

$$J := \int_{\mathcal{D}} \rho(x - x_o) \otimes (x - x_o) dV$$

Total force and moment tensor:

$$f(t) := \int_{\partial\mathcal{D}} q(x, t) dA;$$

$$M(t) := \int_{\partial\mathcal{D}} (x - x_o) \otimes q(x, t) dA$$

# Piola stress and material properties

Frame indifference:

$$S \cdot WF = 0 \quad \forall W \mid \text{sym } W = 0 \quad \Rightarrow \quad \text{skw } SF^T = 0$$

Mooney-Rivlin strain energy (incompressible material):

$$\varphi(F) := c_{10}(\iota_1(C) - 3) + c_{01}(\iota_2(C) - 3)$$

Stress response (energetic + reactive + dissipative):

$$SF^T = \widehat{S}(F)F^T - \pi I + \mu \dot{F}F^{-1}$$

$$\widehat{S}(F) \cdot \dot{F} = \frac{d\varphi(F)}{dt} \quad \Rightarrow \quad \widehat{S}(F)F^T = 2(c_{10}FF^T - c_{01}F^{-T}F^{-1})$$

Dissipation principle:

$$S \cdot \dot{F} - d\varphi(F)/dt \geq 0 \quad \Rightarrow \quad \mu \geq 0$$

# Contact force constitutive laws

Repulsive force:

$$q_r(x, t) = \alpha_r d(x, t)^{-\nu_r} n$$

Damping force:

$$q_d(x, t) = -\beta_d d(x, t)^{-\nu_d} (n \otimes n) \dot{p}(x, t)$$

Frictional force:

$$q_f(x, t) = -\beta_f d(x, t)^{-\nu_f} (I - n \otimes n) \dot{p}(x, t)$$

Adhesive force:

$$q_a(x, t) = -\beta_a (d(x, t)^{-\nu_{aa}} - d(x, t)^{-\nu_{ar}}) n$$

## Contact force constitutive laws

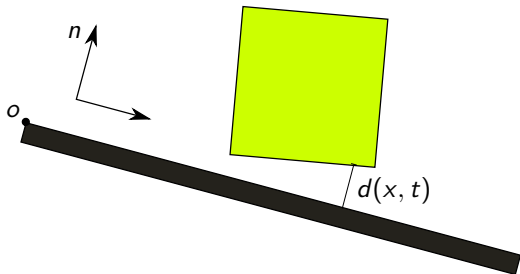
The contact forces are surface forces per unit deformed area:

$$q(x, t) = \sum_j q_j(x, t) k(x, t)$$

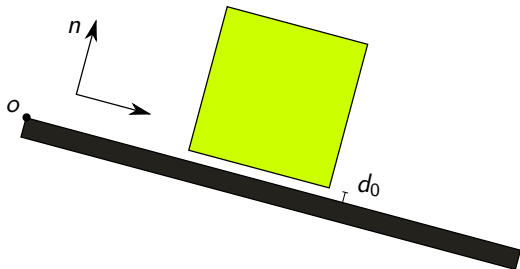
Area change factor:

$$k(x, t) := \|F(t)^{-T} n_{\partial\mathcal{D}}(x)\| \det(F(t))$$

$n_{\partial\mathcal{D}}(x)$  outward unit normal vector



$$d(x, t) := (p(x, t) - o) \cdot n$$



$$d(x, t) := (p(x, t) - o) \cdot n$$

# Contact force constitutive laws

Repulsive force:

$$q_r(x, t) = \alpha_r d(x, t)^{-\nu_r} n$$

Damping force:

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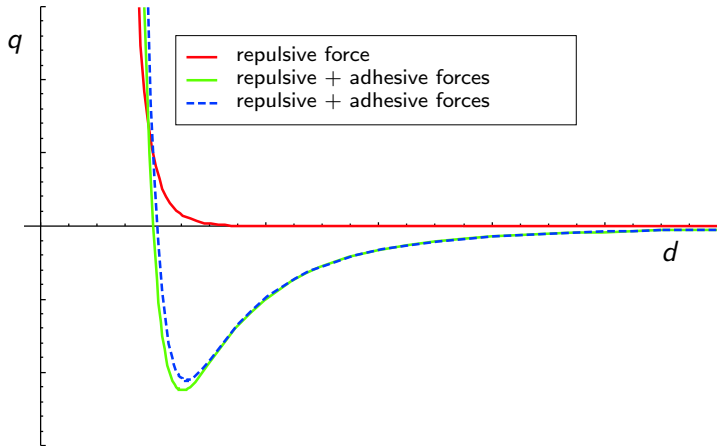
Frictional force:

$$q_f(x, t) = -\beta_f d(x, t)^{-\nu_f} (I - n \otimes n) \dot{p}(x, t)$$

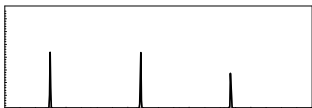
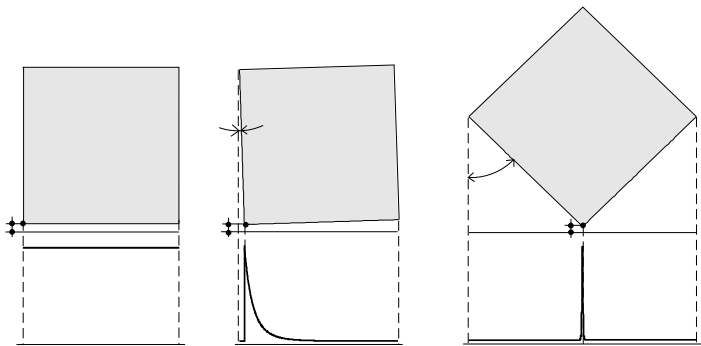
Adhesive force:

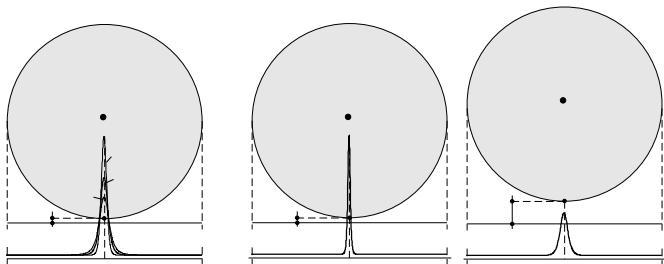
$$q_a(x, t) = -\beta_a (d(x, t)^{-\nu_{aa}} - d(x, t)^{-\nu_{ar}}) n$$



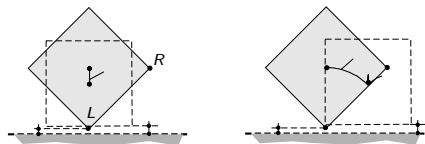


$$\nu_r = 8, \quad \nu_{aa} = 3, \quad \nu_{ar} = 6$$

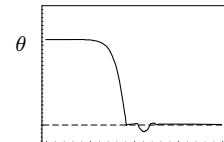
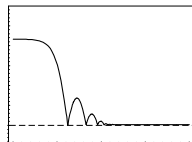
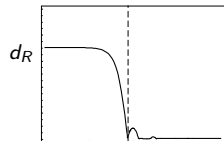
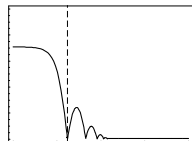
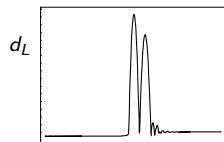
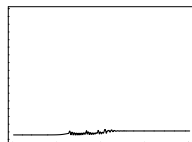




# Numerical simulations



001	011
002	012



$t$

$t$

# Numerical simulations

rocking on a sloping plane

021	022	023
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bouncing and rolling

031	032	033	034	035
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elastic bouncing and oscillations

041	112			
200	214	215	216	217
318	319			

adhesion and detachment

501	502	503	505
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spinning top

3D-101	3D-111
3D-102	3D-112

dice throwing

3D-201	3D-211
3D-202	3D-212

The end







# Appendix

## Cauchy stress

$$T = SF^T \frac{1}{\det F}$$

## Pressure $\pi$

It is the *reactive* part of  $T$ . In an incompressible solid/fluid the velocity fields are said to be *isochoric*. The trace of the velocity gradient turns out to be zero.

A reactive stress, whose power is zero for any isochoric velocity field, has to be a spherical tensor  $-\pi I$ :

$$\pi I \cdot G = \pi \operatorname{tr} G = 0$$

# Appendix

## Mooney-Rivlin

It is a hyperelastic material model used for rubber-like materials as well as for biological tissues.

The *principal invariants* of  $C := FF^T$  are defined as

$$I_1(C) := F \cdot F, \quad I_2(C) := F^* \cdot F^*$$

where  $F^* := F^{-T} \det F$  is the *cofactor* of  $F$ .

## References

- ▶ Nicola Pugno, Towards a Spiderman suit: large invisible cables and self-cleaning releasable superadhesive materials, *J. Phys.: Condens. Matter*, 19, 2007.
- ▶ Alessandro Granaldi, Paolo Decuzzi, The dynamic response of resistive microswitches: switching time and bouncing, *J. Micromech. Microeng.*, 16, 2006.
- ▶ Jiunn-Jong Wu, Adhesive contact between a nano-scale rigid sphere and an elastic half-space, *J. Phys. D: Appl. Phys.*, 39, 2006
- ▶ Z. J. Guo, N. E. McGruer, G. G. Adams, Modeling, simulation and measurement of the dynamic performance of an ohmic contact, electrostatically actuated RF MEMS switch, *J. Micromech. Microeng.*, 17, 2007
- ▶ Makoto Ashino, Alexander Schwarz, Hendrik Hölscher, Udo D. Schwarz, and Roland Wiesendanger, Interpretation of the atomic scale contrast obtained on graphite and single-walled carbon nanotubes in the dynamic mode of atomic force microscopy, *Nanotechnology*, 16, 2005

## Supplementary references

- ▶ Gianfranco Capriz, Paolo Podio-Guidugli, Whence the boundary conditions in modern continuum physics?, *Atti Convegni Lincei n. 210*, 2004
- ▶ Antonio Di Carlo, Actual surfaces versus virtual cuts, *Atti Convegni Lincei n. 210*, 2004