

How the vitreous motion can generate severe tractions on the retina

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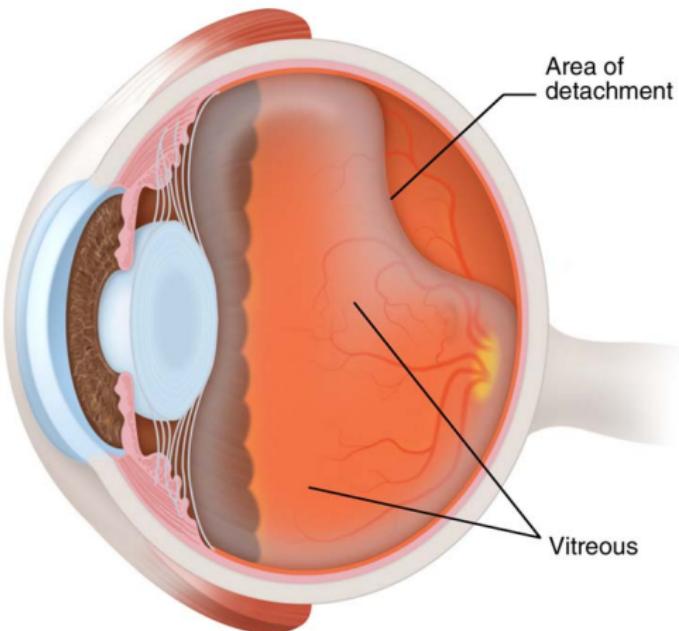
Dipartimento di Ingegneria delle Strutture, delle Acque e del Terreno
Università dell'Aquila - Italy

Genova, February 10, 2009

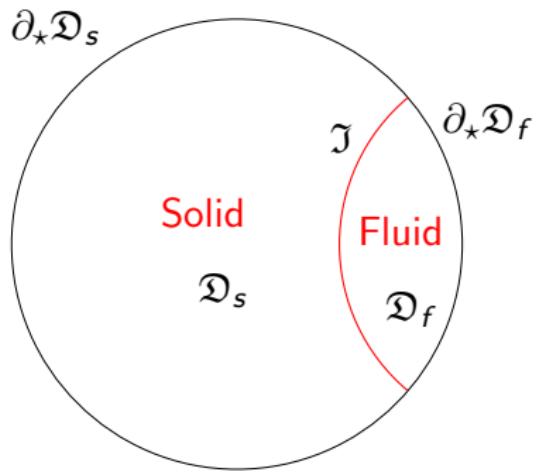
Based on a joint work with:
Rodolfo Repetto, Elisa Colangeli and Alessandro Testa

Dipartimento di Ingegneria delle Strutture, delle Acque e del Terreno
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Posterior vitreous detachment



The mechanical model



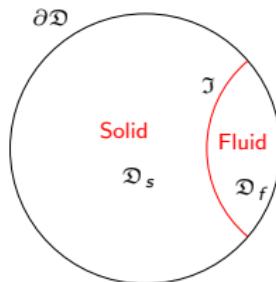
Vitreous chamber after PVD

Balance Principle (solid & fluid)

For any test velocity field \mathbf{w}

$$\int_{\mathfrak{D}} \mathbf{b} \cdot \mathbf{w} \, dV + \int_{\partial\mathfrak{D}} \mathbf{t} \cdot \mathbf{w} \, dA - \int_{\mathfrak{D}} \mathbf{T} \cdot \nabla \mathbf{w} \, dV = 0$$

- b** bulk force per unit volume on \mathfrak{D}
- t** traction per unit area on $\partial\mathfrak{D}$
- T** Cauchy stress tensor

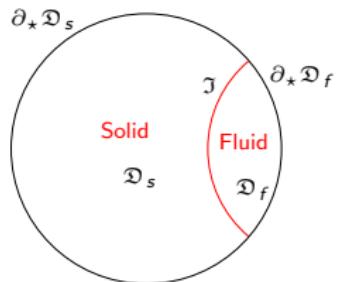


Balance Principle (solid & fluid)

For any test velocity field \mathbf{w}

$$\int_{\mathfrak{D}} \mathbf{b} \cdot \mathbf{w} \, dV + \int_{\partial\mathfrak{D}} \mathbf{t} \cdot \mathbf{w} \, dA - \int_{\mathfrak{D}} \mathbf{T} \cdot \nabla \mathbf{w} \, dV - \int_{\mathfrak{I}} \mathbf{t}^* \cdot [\![\mathbf{w}]\!] \, dA = 0$$

- b** bulk force per unit volume on \mathfrak{D}
- t** traction per unit area on $\partial\mathfrak{D}$
- T** Cauchy stress tensor
- \mathbf{t}^*** interface stress

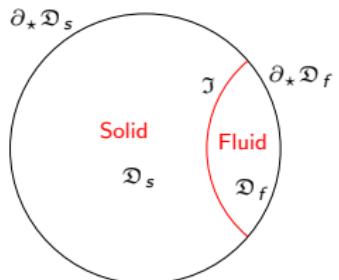


Balance Principle (fluid)

For any test velocity field \mathbf{w}

$$\int_{\mathfrak{D}_f} \mathbf{b}_f \cdot \mathbf{w}_f \, dV + \int_{\partial_* \mathfrak{D}_f} \mathbf{t}_f \cdot \mathbf{w}_f \, dA + \int_{\mathfrak{I}} \mathbf{t}_f \cdot \mathbf{w}_f \, dA - \int_{\mathfrak{D}_f} \mathbf{T}_f \cdot \nabla \mathbf{w}_f \, dV = 0$$

- \mathbf{b}_f bulk force per unit volume on \mathfrak{D}_f
- \mathbf{t}_f traction per unit area on $\partial \mathfrak{D}_f$
- \mathbf{T}_f Cauchy stress tensor

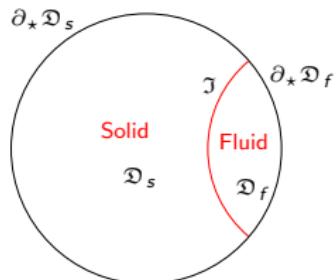


Balance Principle (solid)

For any test velocity field \mathbf{w}

$$\int_{\mathfrak{D}_s} \mathbf{b}_s \cdot \mathbf{w}_s \, dV + \int_{\partial_* \mathfrak{D}_s} \mathbf{t}_s \cdot \mathbf{w}_s \, dA + \int_{\mathfrak{I}} \mathbf{t}_s \cdot \mathbf{w}_s \, dA - \int_{\mathfrak{D}_s} \mathbf{T}_s \cdot \nabla \mathbf{w}_s \, dV = 0$$

- \mathbf{b}_s bulk force per unit volume on \mathfrak{D}_s
- \mathbf{t}_s traction per unit area on $\partial \mathfrak{D}_s$
- \mathbf{T}_s Cauchy stress tensor

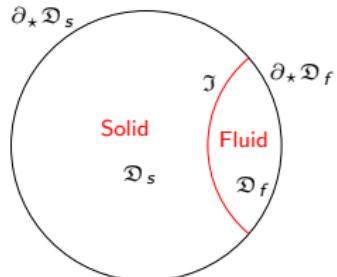


Balance Principle (solid & membrane)

For any test velocity field \mathbf{w}

$$\int_{\mathfrak{D}_s} \mathbf{b}_s \cdot \mathbf{w}_s \, dV + \int_{\partial_* \mathfrak{D}_s} \mathbf{t}_s \cdot \mathbf{w}_s \, dA + \int_{\mathfrak{I}} \mathbf{t}_s \cdot \mathbf{w}_s \, dA - \int_{\mathfrak{D}_s} \mathbf{T}_s \cdot \nabla \mathbf{w}_s \, dV \\ - \int_{\mathfrak{I}} \mathbf{N}_s \cdot \nabla^* \mathbf{w}_s \, dA = 0$$

- \mathbf{b}_s bulk force per unit volume on \mathfrak{D}_s
- \mathbf{t}_s traction per unit area on $\partial_* \mathfrak{D}_s$
- \mathbf{T}_s Cauchy stress tensor
- \mathbf{N}_s Membrane stress tensor



Balance Equations (solid & membrane)

$$\operatorname{div} \mathbf{T}_s + \mathbf{b}_s = 0$$

on \mathfrak{D}_s

$$\mathbf{t}_s = \mathbf{T}_s \mathbf{n}$$

on $\partial_* \mathfrak{D}_s$

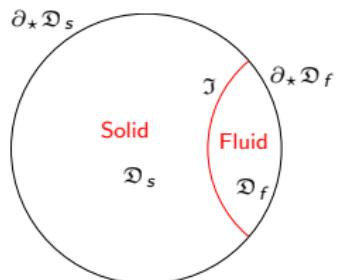
$$\operatorname{div}^* \mathbf{N}_s + \mathbf{t}_s - \mathbf{T}_s \mathbf{n} = 0$$

on \mathfrak{I}

$$\mathbf{t}_{\partial \mathfrak{I}} = \mathbf{N}_s \mathbf{n}_{\partial \mathfrak{I}}$$

on $\partial \mathfrak{I}$

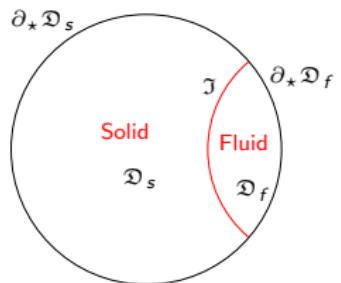
$\mathbf{t}_{\partial \mathfrak{I}}$ traction on $\partial \mathfrak{I}$
 \mathbf{N}_s membrane stress tensor



Boundary conditions (solid & fluid)

$$\mathbf{t}_s = \mathbf{T}_f \mathbf{n}_s \quad \text{on } \mathfrak{I}$$

$$\mathbf{v}_s = \mathbf{v}_f \quad \text{on } \mathfrak{I}$$



Material response

$$\mathbf{T}_s = -p_s \mathbf{I} + \hat{\mathbf{T}}_s(\mathbf{F}) + 2\mu_s \operatorname{sym} \nabla \mathbf{v}_s$$

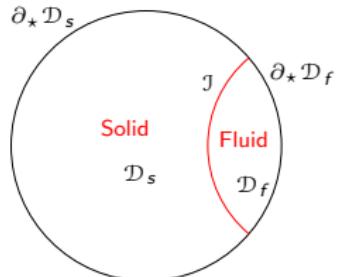
$$\mathbf{T}_f = -p_f \mathbf{I} + 2\mu_f \operatorname{sym} \nabla \mathbf{v}_f$$

Balance Principle on the (solid) *paragon shape*

For any test velocity field w

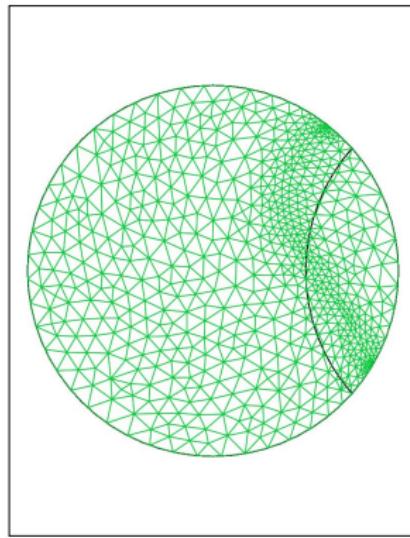
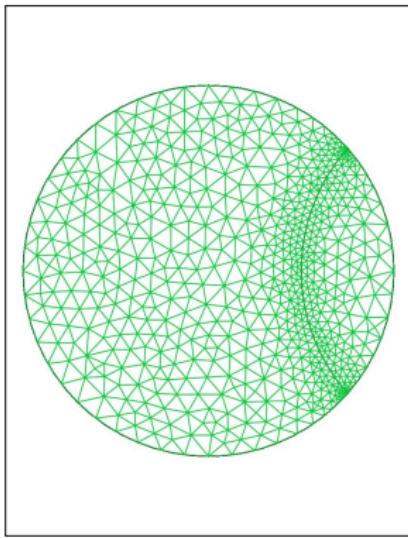
$$\int_{\mathcal{D}_s} \mathbf{b}_s \cdot \mathbf{w}_s \, dV + \int_{\partial_* \mathcal{D}_s} \mathbf{t}_s \cdot \mathbf{w}_s \, dA + \int_{\mathcal{J}} \mathbf{t}_s \cdot \mathbf{w}_s \, dA - \int_{\mathcal{D}_s} \mathbf{S}_s \cdot \nabla \mathbf{w}_s \, dV \\ - \int_{\mathcal{J}} \mathbf{N}_s \cdot \nabla^* \mathbf{w}_s \, dA = 0$$

- \mathbf{b}_s bulk force per unit volume on \mathcal{D}_s
- \mathbf{t}_s traction per unit area on $\partial_* \mathcal{D}_s$
- \mathbf{S}_s Piola Kirchhoff stress tensor
- \mathbf{N}_s Membrane Piola Kirchhoff stress tensor



Moving grid

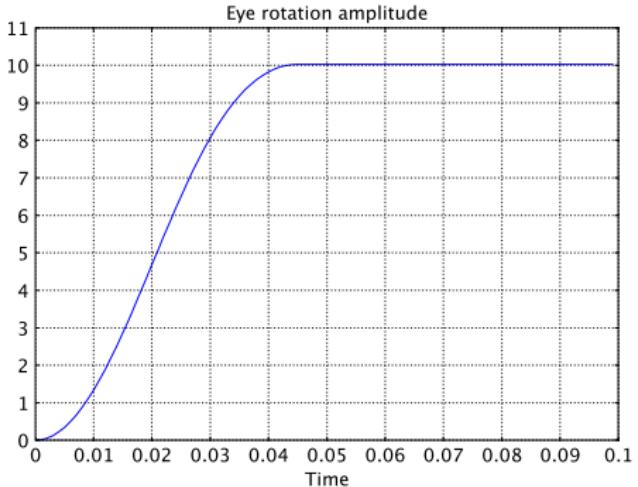
$$\gamma : \mathcal{D} \rightarrow \mathfrak{D}$$



$$\gamma_s = \phi_s$$

$$\Delta\gamma_f = 0$$

Saccadic movement



Constitutive parameters

Author	Parameter	
Bettelheim et al. (1976)	Dynamic extensional moduli (bovine)	3-4 Pa
Zimmermann (1980)	Elastic shear modulus G (human)	0.05 Pa
Buchsbaum et al. (1984)	Dynamic shear storage G' and loss G'' (human)	$\ll 1.5$ Pa
	Dynamic shear storage G' and loss G'' (porcine)	1-1.5 Pa
Lee et al. (1992)	Internal elastic shear modulus G_k (human)	1.2 Pa
	Internal viscosity η_k	0.489 Pa s
	Instantaneous elastic compliance $J_m = 1/G_m$ (human)	0.3 Pa ⁻¹
Nickerson et al. (2008)	Dynamic shear storage G' (bovine) - Initial value	32 Pa
	Dynamic shear storage G' (bovine) - Final value	7 Pa
	Dynamic shear loss G'' (bovine) - Initial value	17 Pa
	Dynamic shear loss G'' (bovine) - Final value	2.2 Pa
	Dynamic shear storage G' (porcine) - Initial value	10 Pa
	Dynamic shear storage G' (porcine) - Final value	2.8 Pa
	Dynamic shear loss G'' (porcine) - Initial value	3.9 Pa
	Dynamic shear loss G'' (porcine) - Final value	0.7 Pa

Eye radius and constitutive parameters

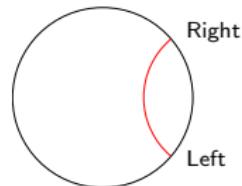
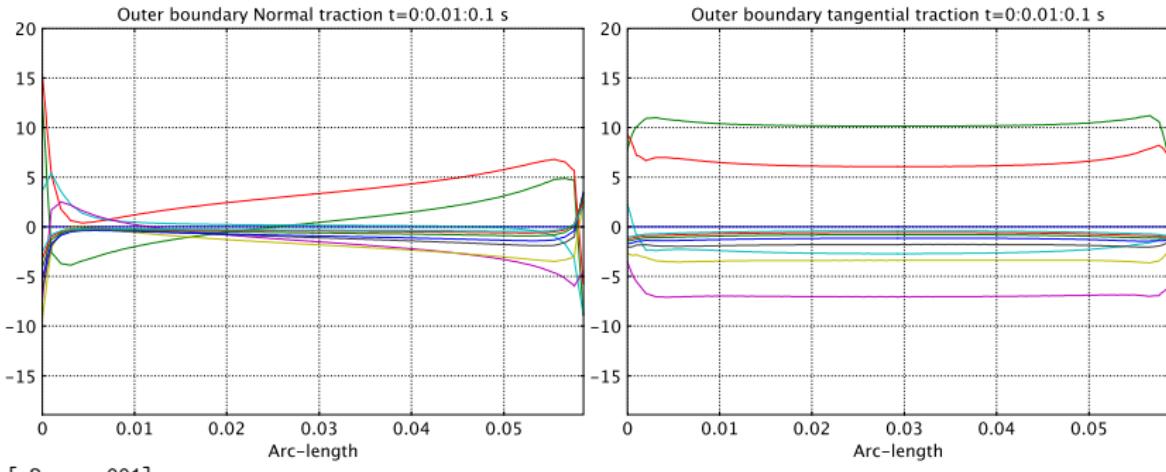
Radius $R = 0.012 \text{ m}$

Fluid viscosity $\mu = 10^{-3} \text{ Pa s}$

Mass density $\rho_s = \rho_f = 1000 \text{ kg/m}^3$

Boundary traction
for different values of the *solid elastic modulus*

Boundary traction (vs. solid elastic modulus)

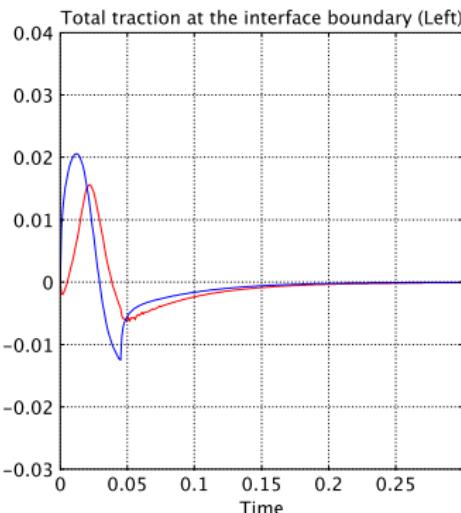


$$c_{01} := 1.0 \text{ Pa}$$

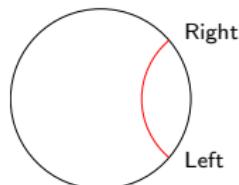
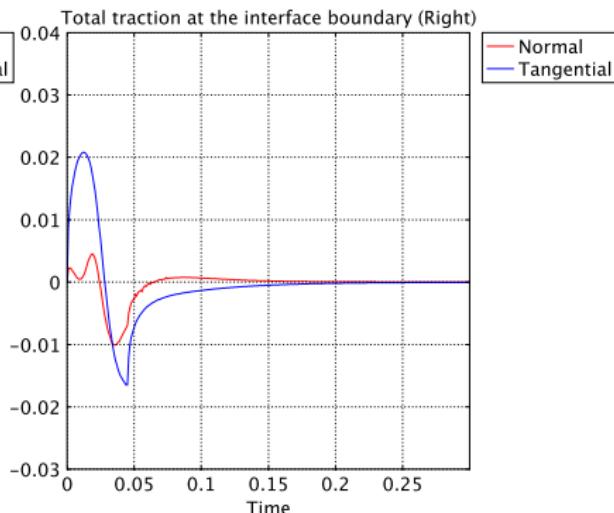
$$m_{01} := 1.0 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



[a2_case_005]

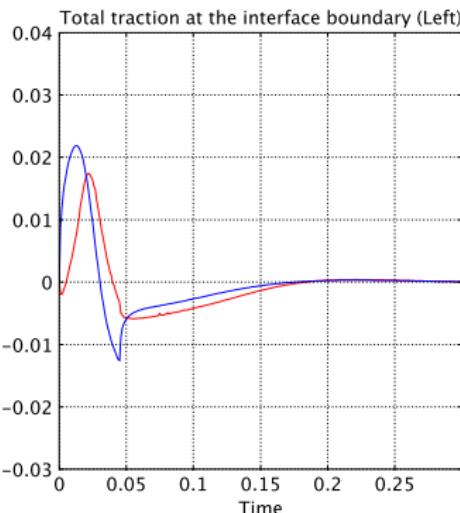


$$c_{01} := 0.5 \text{ Pa}$$

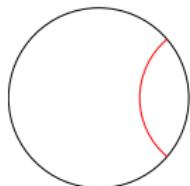
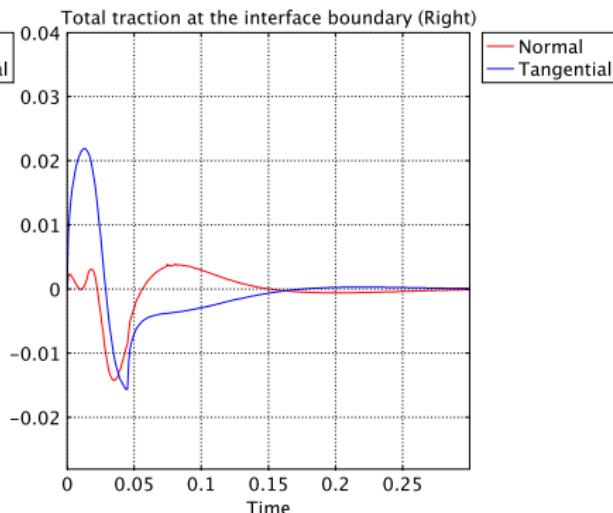
$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



[a2_case_008]

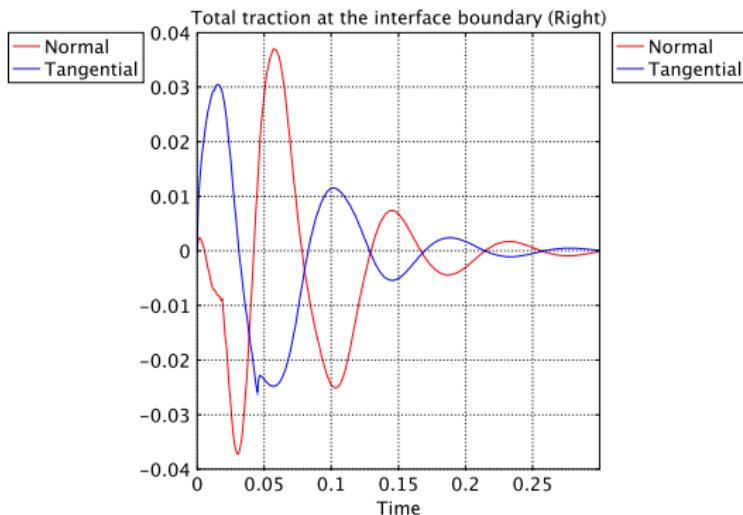
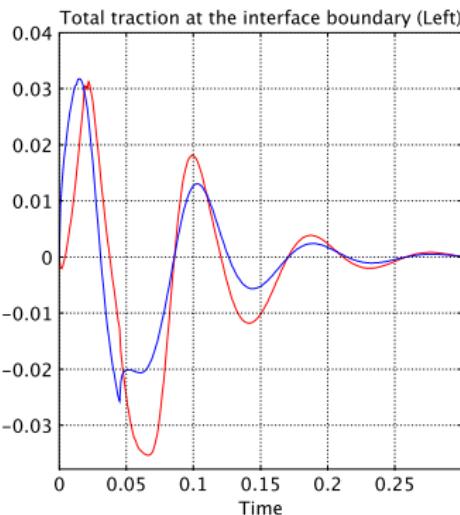


$$c_{01} := 2.5 \text{ Pa}$$

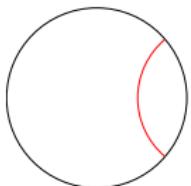
$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



[a2_case_012]

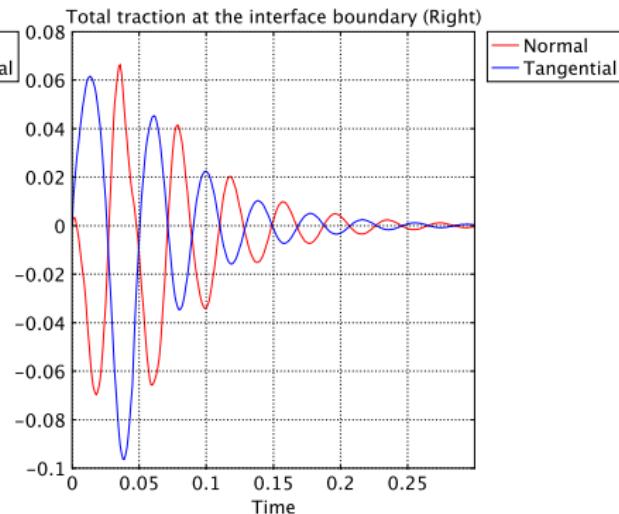
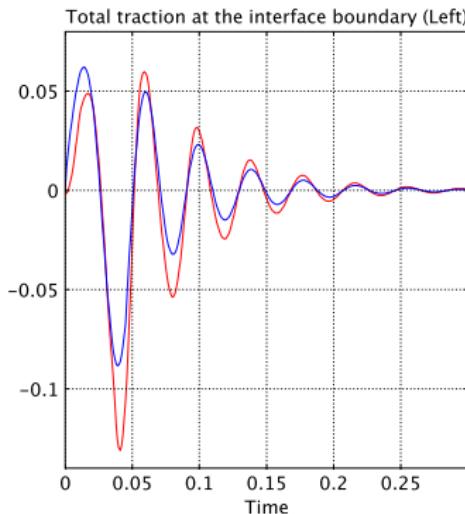


$$c_{01} := 20 \text{ Pa}$$

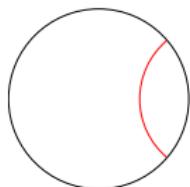
$$m_{01} := 20 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



[a2_case_013]

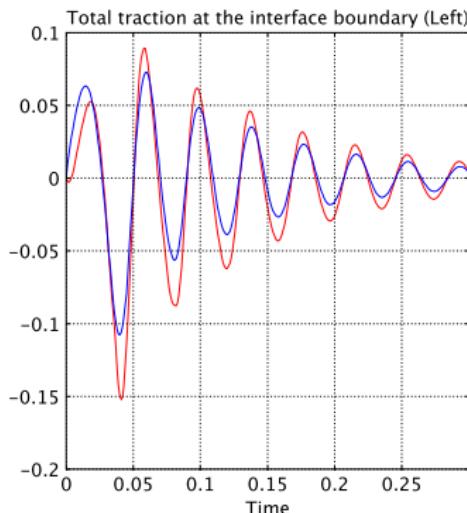


$$c_{01} := 100 \text{ Pa}$$

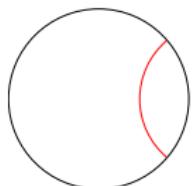
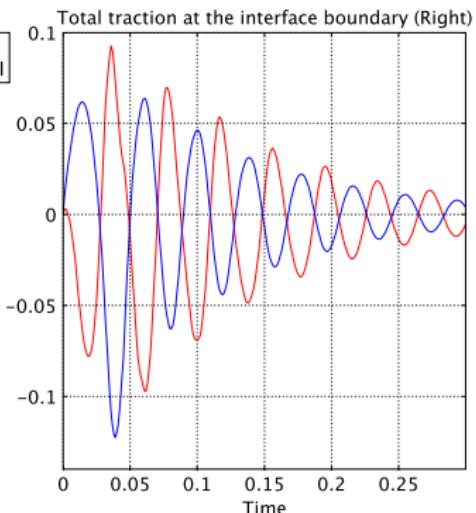
$$m_{01} := 100 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



[a2_case_014]



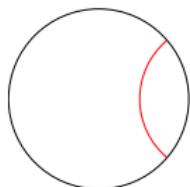
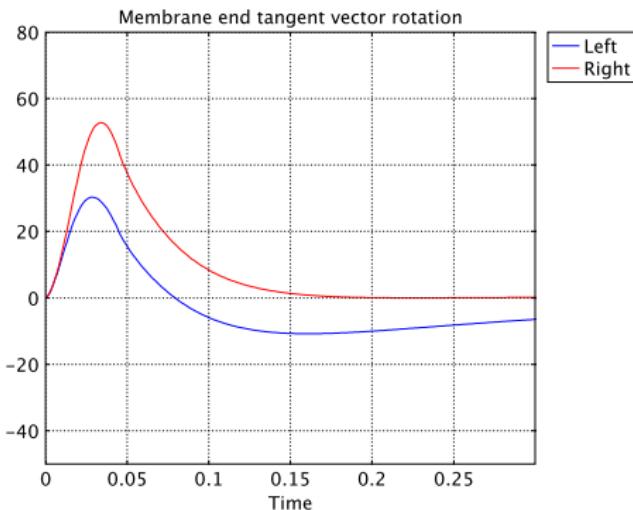
$$c_{01} := 100 \text{ Pa}$$

$$m_{01} := 100 \text{ Pa}$$

$$\mu_s := 0.3 \text{ Pa s}$$

Membrane oscillations
for different values of the *solid elastic modulus*

Membrane oscillations (vs. solid elastic modulus)

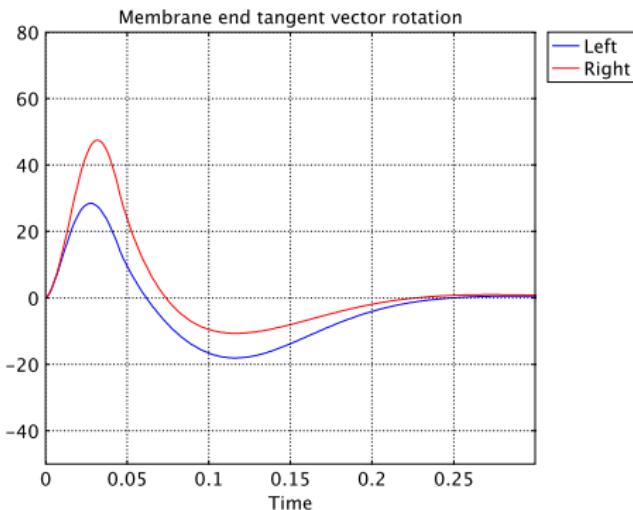


$$c_{01} := 0.5 \text{ Pa}$$

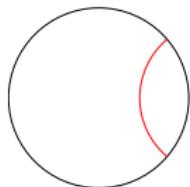
$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Membrane oscillations (vs. solid elastic modulus)



[a2_case_008]

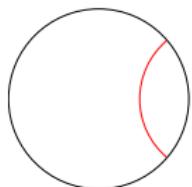
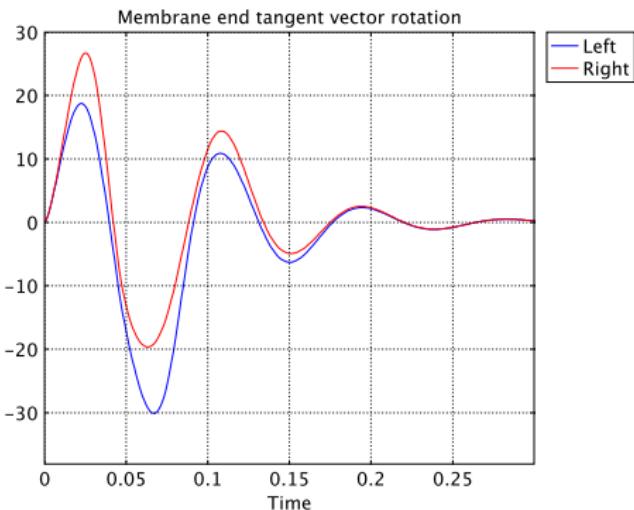


$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Membrane oscillations (vs. solid elastic modulus)

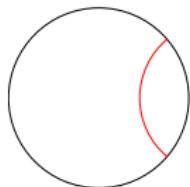
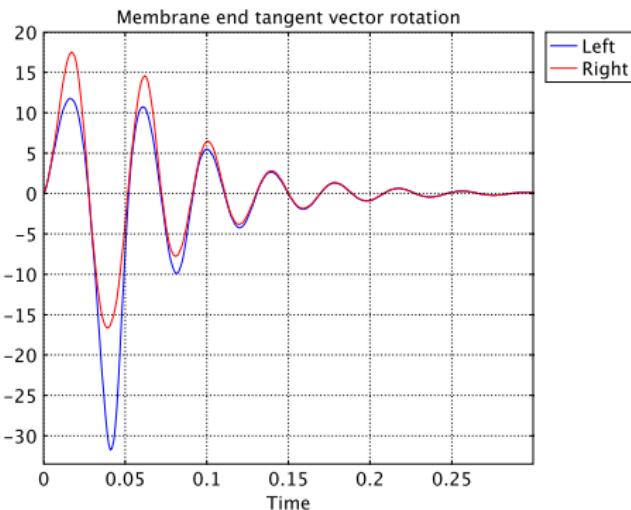


$$c_{01} := 20 \text{ Pa}$$

$$m_{01} := 20 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Membrane oscillations (vs. solid vitreous elastic modulus)

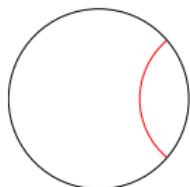
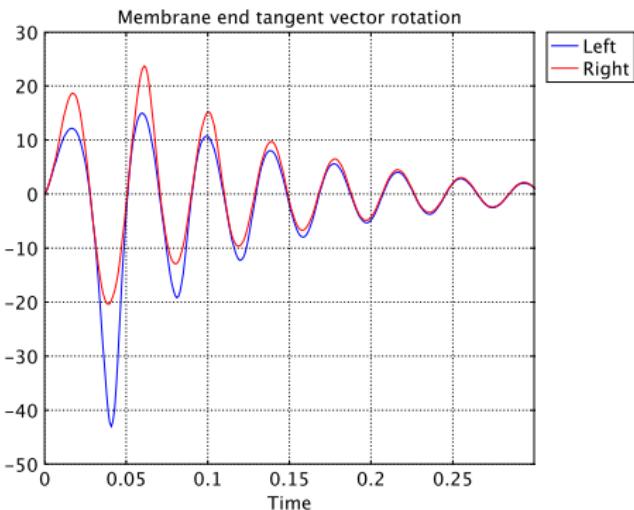


$$c_{01} := 100 \text{ Pa}$$

$$m_{01} := 100 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Membrane oscillations (vs. solid vitreous elastic modulus)



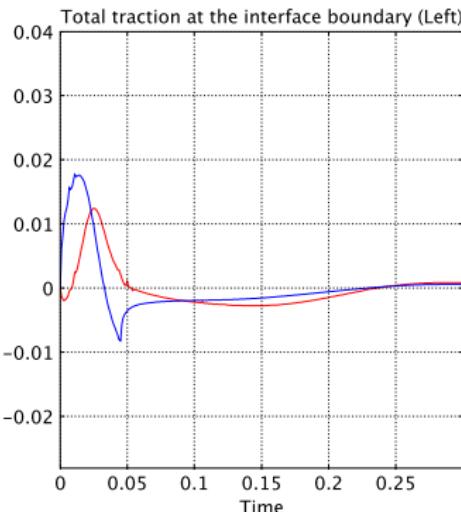
$$c_{01} := 100 \text{ Pa}$$

$$m_{01} := 100 \text{ Pa}$$

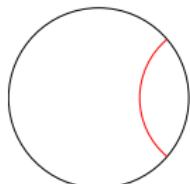
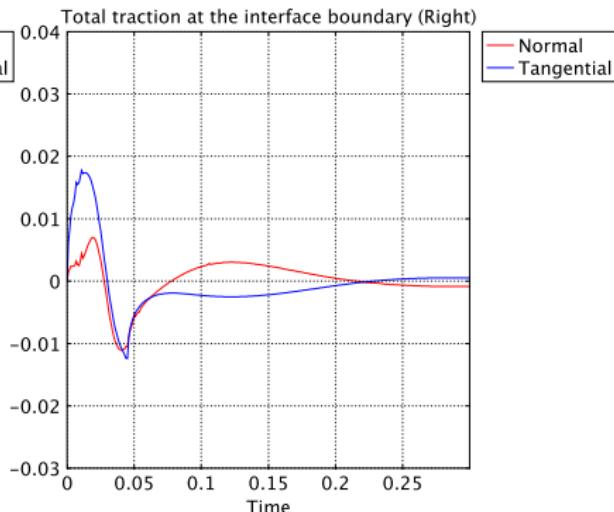
$$\mu_s := 0.3 \text{ Pa s}$$

Boundary traction
for different values of the *solid viscosity*

Boundary traction (vs. solid viscosity)



[a2_case_009]

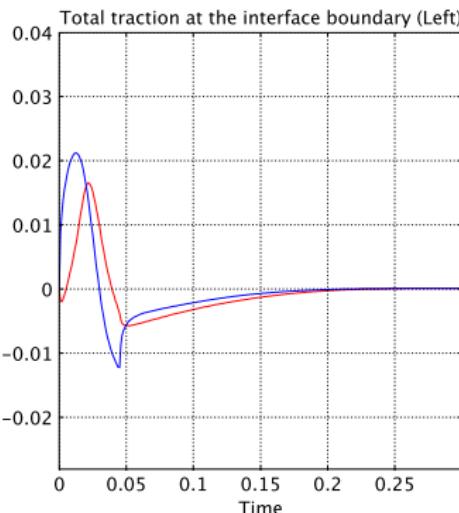


$$c_{01} := 1.5 \text{ Pa}$$

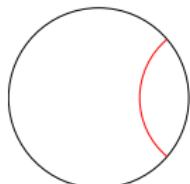
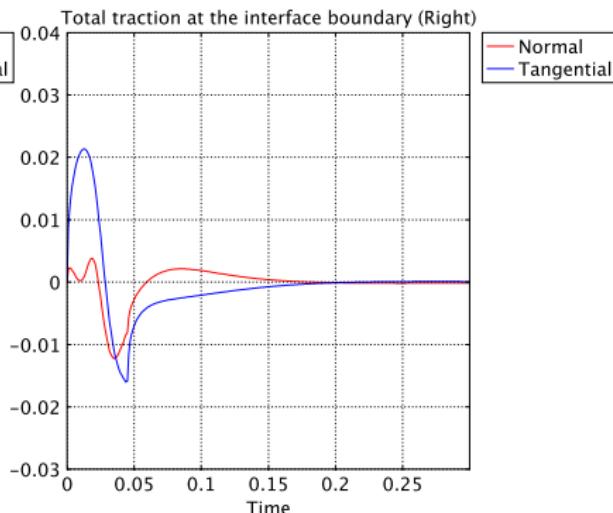
$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.25 \text{ Pa s}$$

Boundary traction (vs. solid viscosity)



[a2_case_006]

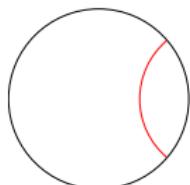
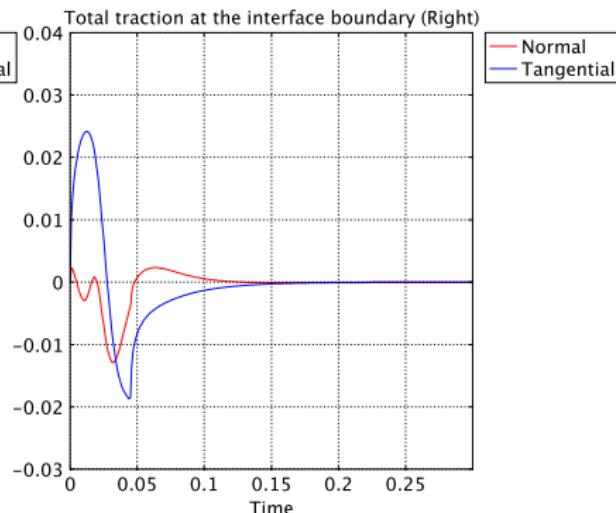
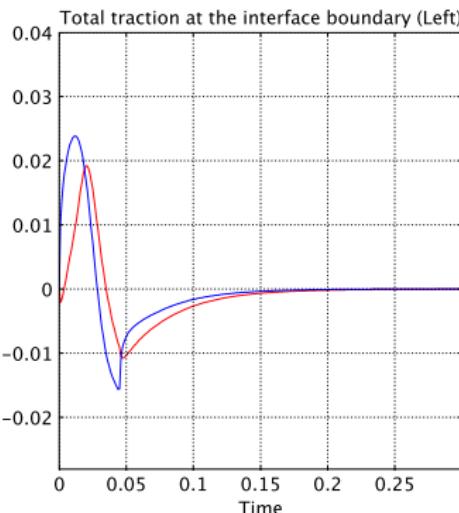


$$c_{01} := 1.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Boundary traction (vs. solid viscosity)

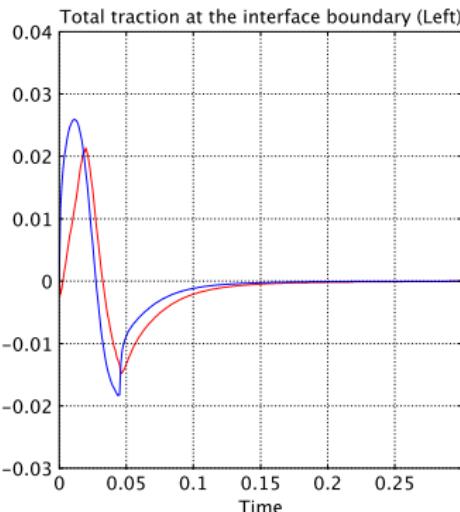


$$c_{01} := 1.5 \text{ Pa}$$

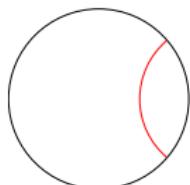
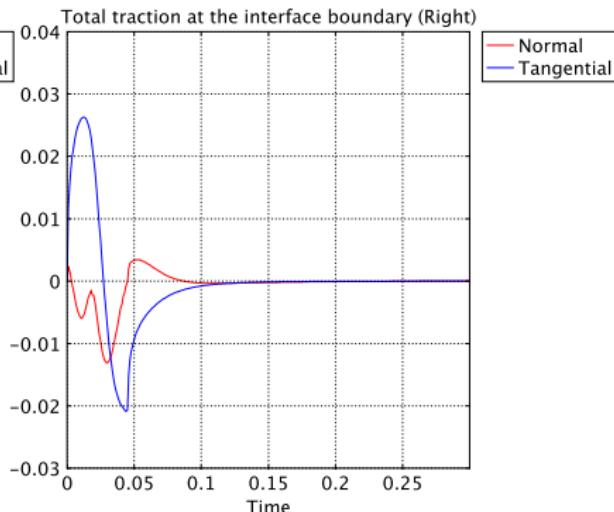
$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.75 \text{ Pa s}$$

Boundary traction (vs. solid viscosity)



[a2_case_011]



$$c_{01} := 1.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

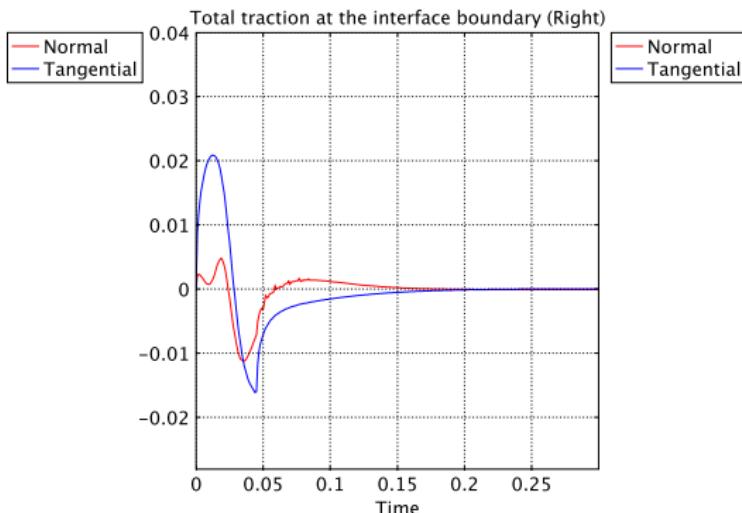
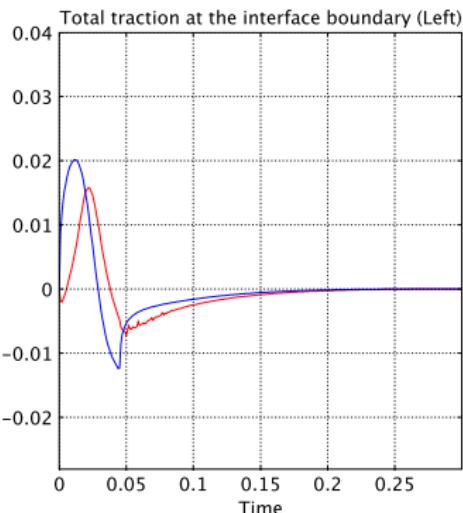
$$\mu_s := 1.00 \text{ Pa s}$$

Damping factors and natural frequencies

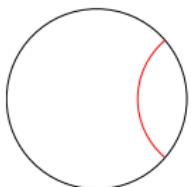
Case	c_{01} (Pa)	m_{01} (Pa)	μ (Pa s)	λ_1			λ_2			λ_3		
008	2.5	10	0.5	-32.90	\pm	$15.13i$	-34.31	\pm	$16.04i$	-16.93	\pm	$19.18i$
009	1.5	10	0.25	-8.64	\pm	$17.95i$	-16.88	\pm	$23.15i$	-17.14	\pm	$23.20i$
012	20	20	0.5	-17.49	\pm	$71.11i$	-33.87	\pm	$97.69i$	-33.60	\pm	$98.14i$
013	100	100	0.5	-17.77	\pm	$163.42i$	-34.08	\pm	$229.22i$	-33.66	\pm	$229.60i$
014	100	100	0.3	-11.03	\pm	$164.02i$	-20.75	\pm	$230.81i$	-20.28	\pm	$231.17i$

Boundary traction
for different values of the *membrane elastic modulus*

Boundary traction (vs. membrane elastic modulus)



[a2_case_001]

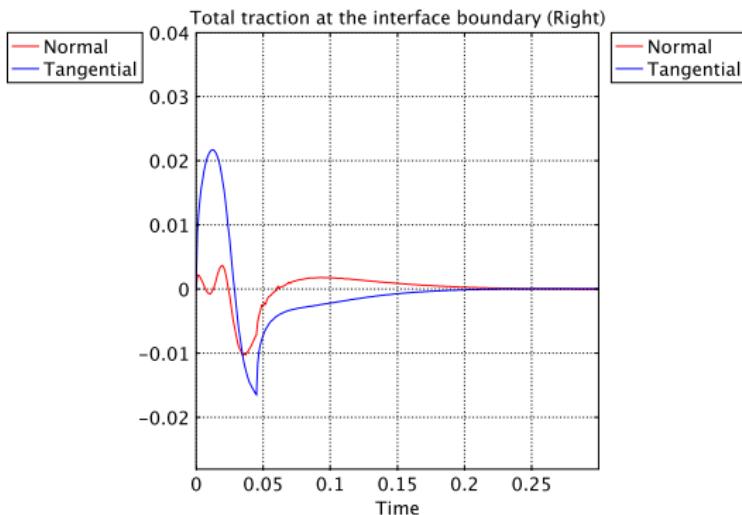
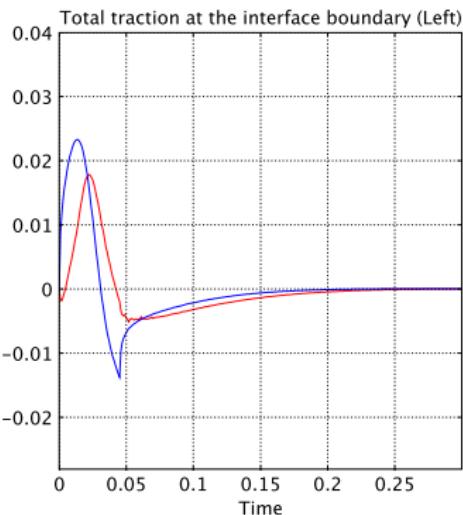


$$c_{01} := 1.0 \text{ Pa}$$

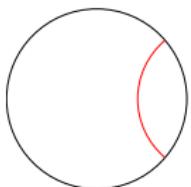
$$m_{01} := 1.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Boundary traction (vs. membrane elastic modulus)



[a2_case_004]

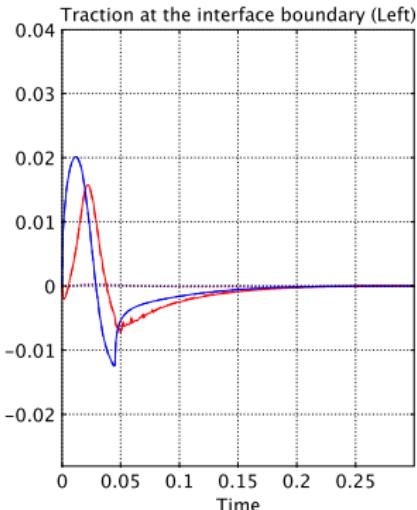


$$c_{01} := 1.0 \text{ Pa}$$

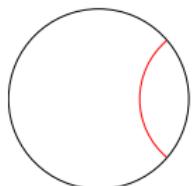
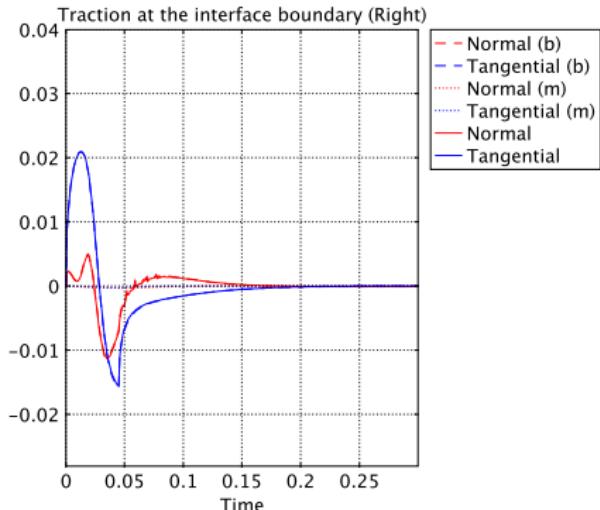
$$m_{01} := 50.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Boundary traction (vs. membrane elastic modulus)



[a2_case_001]

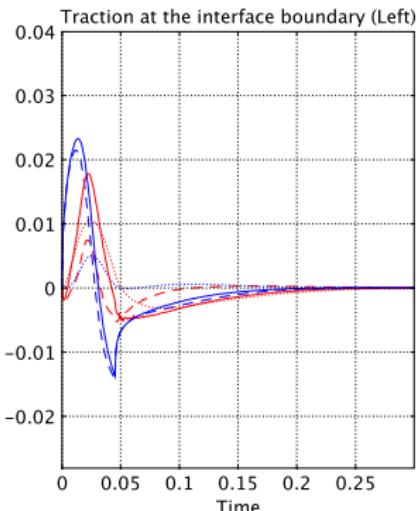


$$c_{01} := 1.0 \text{ Pa}$$

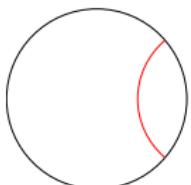
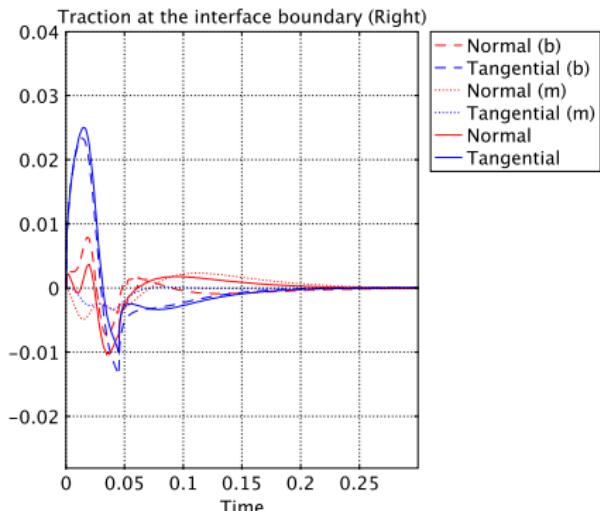
$$m_{01} := 1.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Boundary traction (vs. membrane elastic modulus)



[a2_case_004]

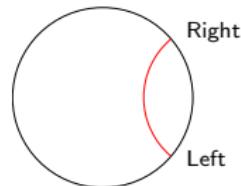
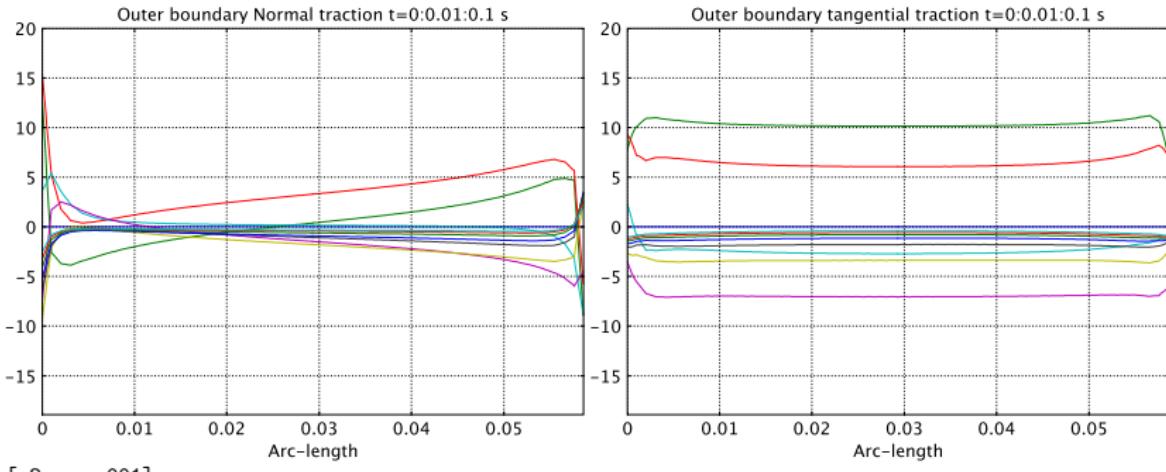


$$c_{01} := 1.0 \text{ Pa}$$

$$m_{01} := 50.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)

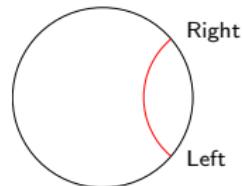
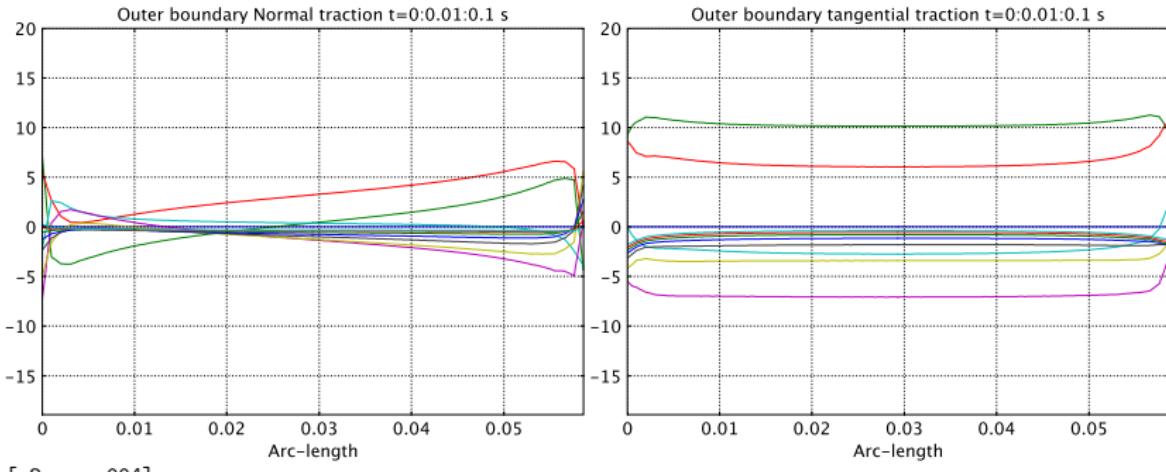


$$c_{01} := 1.0 \text{ Pa}$$

$$m_{01} := 1.0 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Boundary traction (vs. solid elastic modulus)



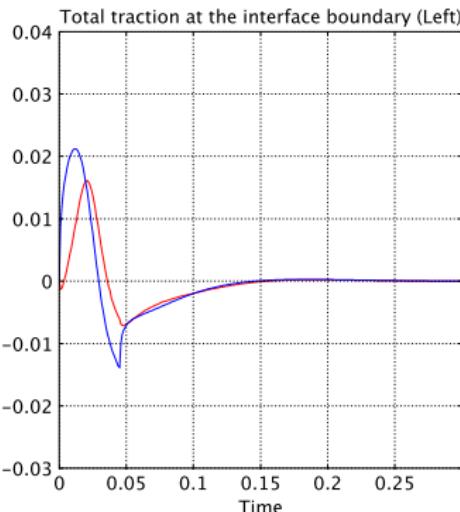
$$c_{01} := 1.0 \text{ Pa}$$

$$m_{01} := 50 \text{ Pa}$$

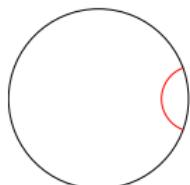
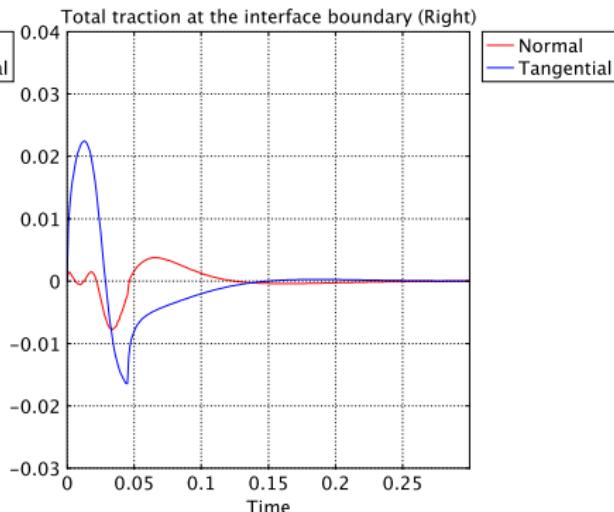
$$\mu_s := 0.5 \text{ Pa s}$$

Comparing different PVD conformations

Different PVD conformations



[a1_case_008]

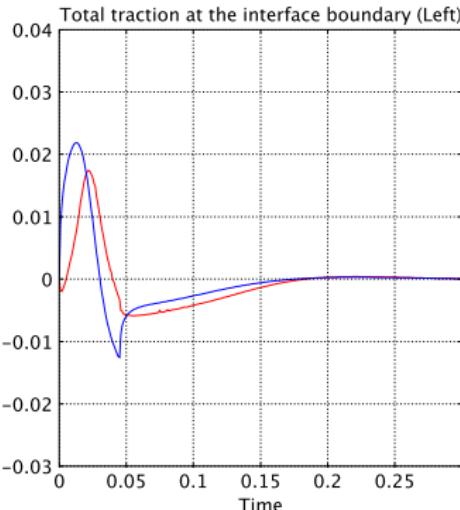


$$c_{01} := 2.5 \text{ Pa}$$

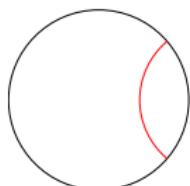
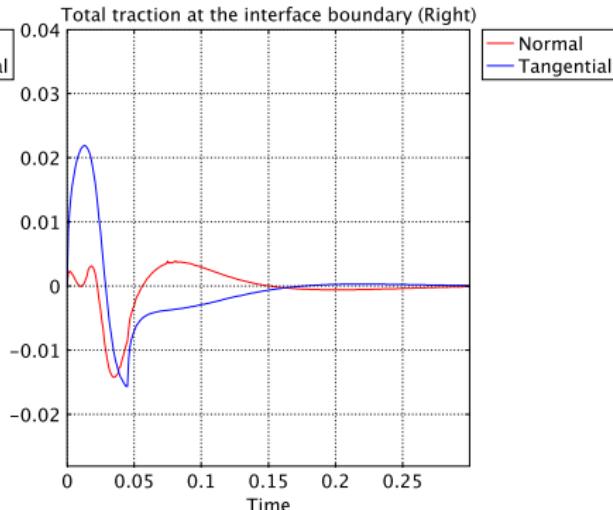
$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations



[a2_case_008]

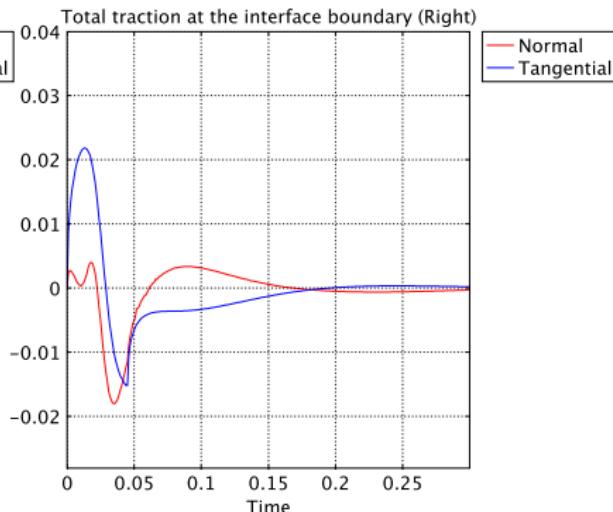
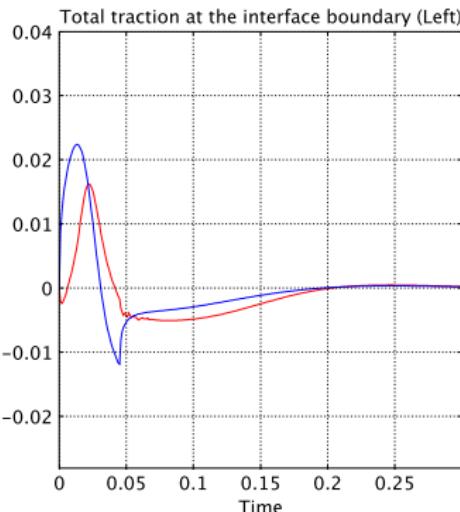


$$c_{01} := 2.5 \text{ Pa}$$

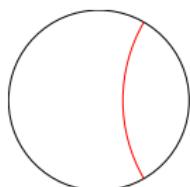
$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations



[a3_case_008]

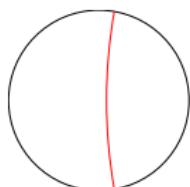
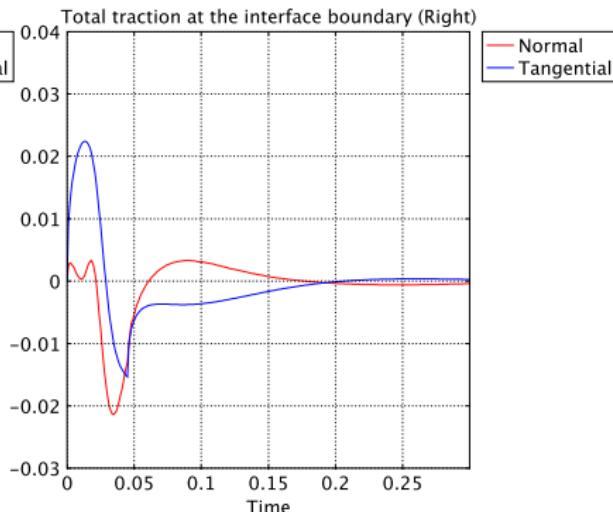
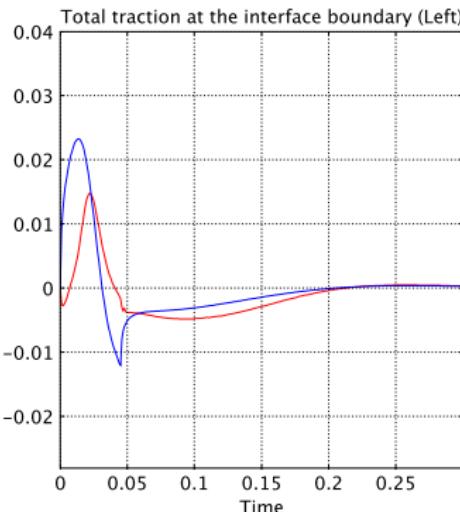


$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations

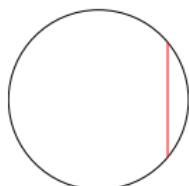
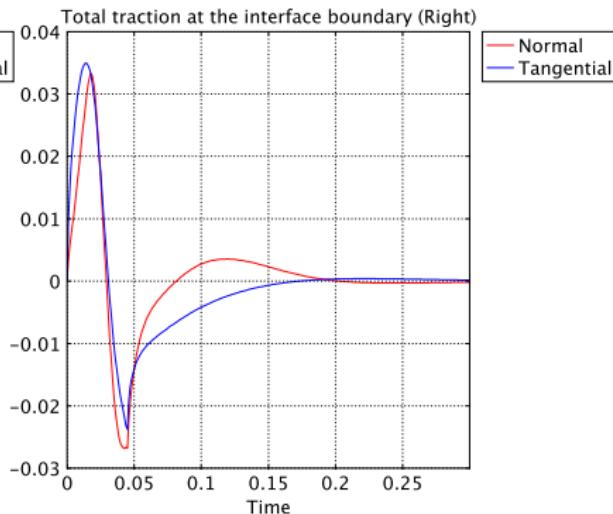
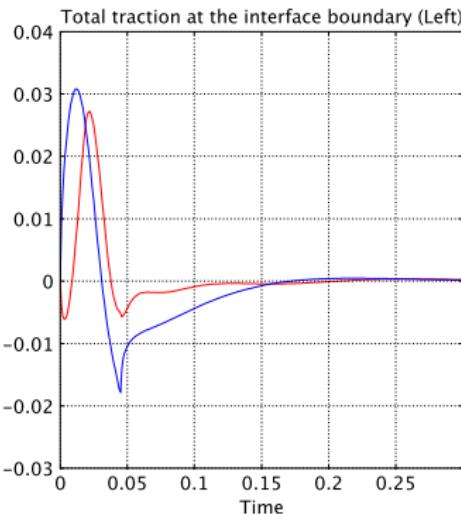


$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations

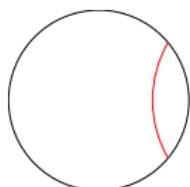
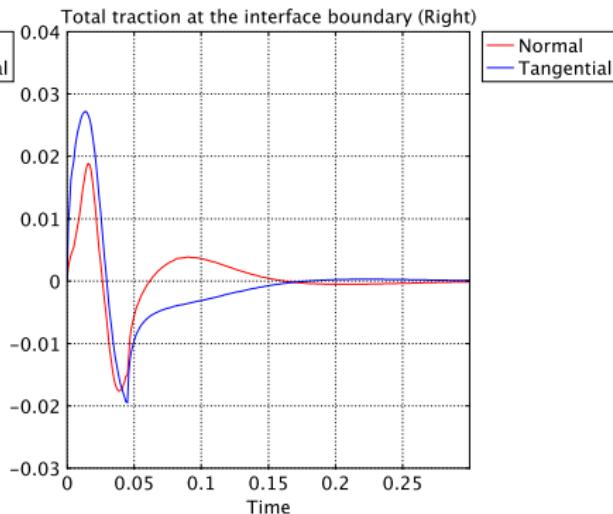
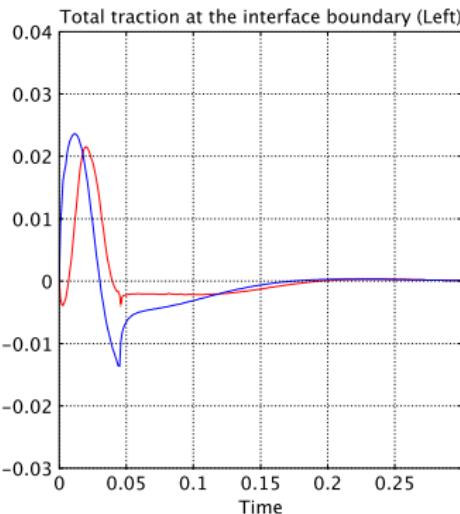


$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations

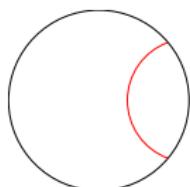
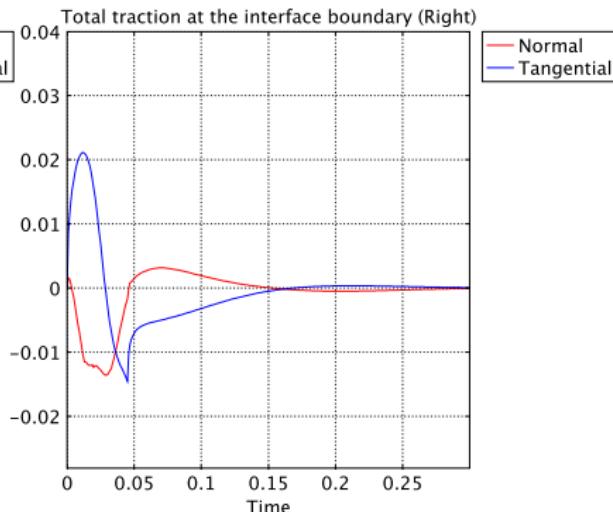
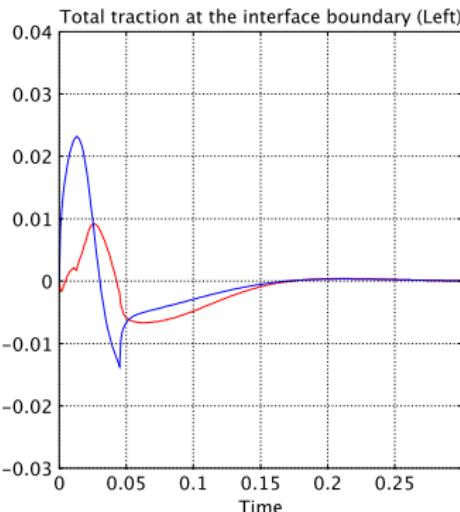


$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

Different PVD conformations



$$c_{01} := 2.5 \text{ Pa}$$

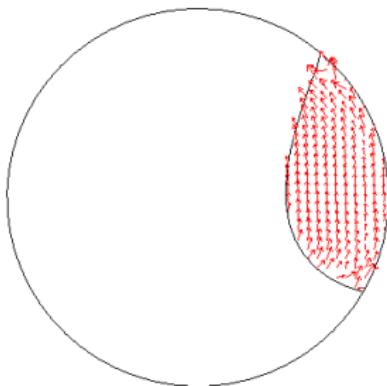
$$m_{01} := 10.0 \text{ Pa}$$

$$\mu_s := 0.50 \text{ Pa s}$$

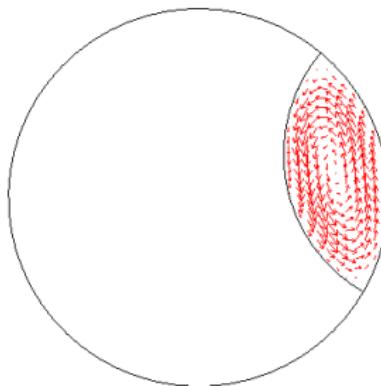
Velocity field and pressure in the fluid part of the vitreous

Fluid vitreous velocity field

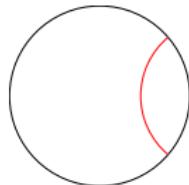
Fluid velocity field at time=0.045 s



Fluid velocity field at time=0.9 s



[a2_case_003]



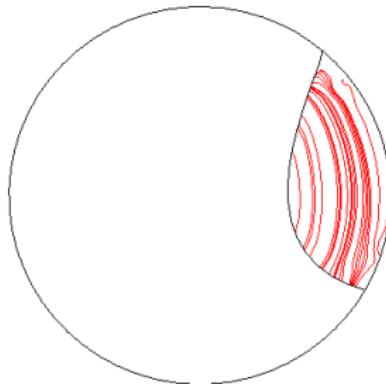
$$c_{01} := 0.5 \text{ Pa}$$

$$m_{01} := 10 \text{ Pa}$$

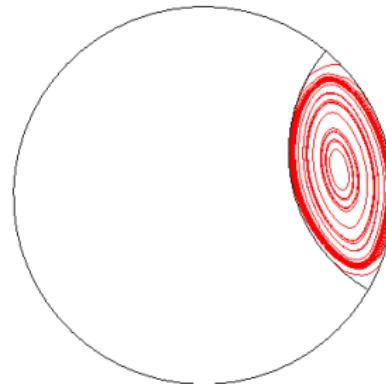
$$\mu_s := 0.5 \text{ Pa s}$$

Fluid vitreous velocity field

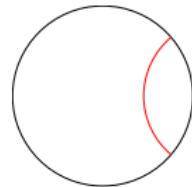
Streamlines of the fluid flow at time=0.045 s



Streamlines of the fluid flow at time=0.9 s



[a2_case_003]



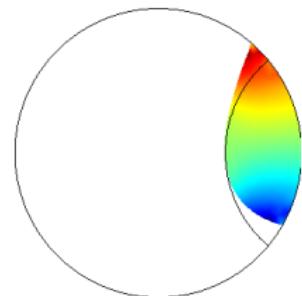
$$c_{01} := 0.5 \text{ Pa}$$

$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

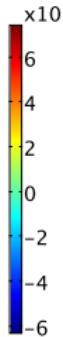
Fluid vitreous pressure field

Fluid pressure field at time=0.045 s

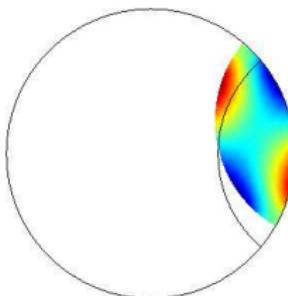


[a2_case_003]

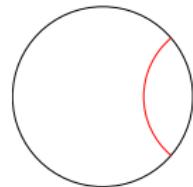
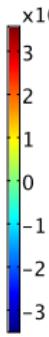
Max: 7.396e-5
 $\times 10^{-5}$



Fluid pressure field at time=2 s



Max: 3.566e-5
 $\times 10^{-5}$

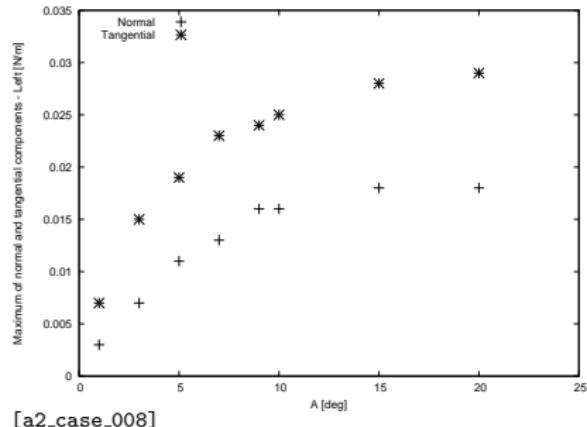


$$c_{01} := 0.5 \text{ Pa}$$

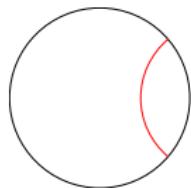
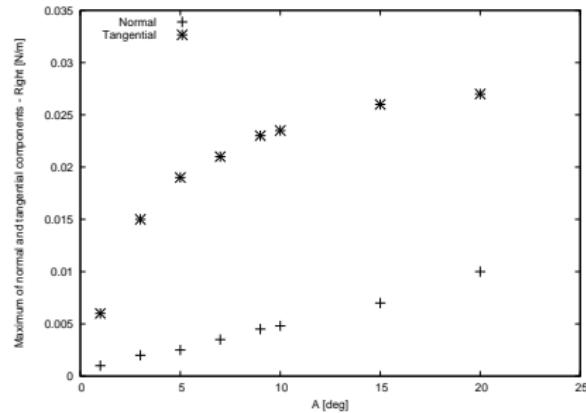
$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Increasing saccade amplitudes



[a2_case_008]



$$c_{01} := 2.5 \text{ Pa}$$

$$m_{01} := 10 \text{ Pa}$$

$$\mu_s := 0.5 \text{ Pa s}$$

Appendix: Piola stress and material properties

Frame indifference

$$S \cdot WF = 0 \quad \forall W \mid \text{sym } W = 0 \quad \Rightarrow \quad \text{skw } SF^T = 0$$

Mooney-Rivlin strain energy (incompressible material):

$$\varphi(F) := c_{10}(\iota_1(C) - 3) + c_{01}(\iota_2(C) - 3)$$

Stress response (energetic + reactive + dissipative):

$$SF^T = \hat{S}(F)F^T - \pi I + \mu \dot{F}F^{-1}$$

$$\hat{S}(F) \cdot \dot{F} = \frac{d\varphi(F)}{dt} \quad \Rightarrow \quad \hat{S}(F) F^T = 2(c_{10}FF^T - c_{01}F^{-T}F^{-1})$$

Dissipation principle:

$$S \cdot \dot{F} - d\varphi(F)/dt \geq 0 \quad \Rightarrow \quad \mu \geq 0$$

Appendix: Pressure

Pressure π is the *reactive* part of \mathbf{T} . In an incompressible solid/fluid the velocity fields are said to be *isochoric*. The trace of the velocity gradient turns out to be zero.

A reactive stress, whose power is zero for any isochoric velocity field, has to be a spherical tensor $-\pi \mathbf{I}$:

$$\pi \mathbf{I} \cdot \mathbf{G} = \pi \operatorname{tr} \mathbf{G} = 0$$