

(25-26)₅ Monday [2014-03-24] A1.3
16:00-18:00

$$W a = \lambda a \Rightarrow \lambda = 0$$

$$\omega = a / \|a\|$$

$$W \omega = 0 \quad \text{vol}(\omega, u, v) = \omega \times u \cdot v \quad \forall v$$

$\text{vol}(e_1, e_2, e_3) = 1$

$$\text{vol}(\omega, u, v) = (*\omega)u \cdot v \quad \forall v, \forall u, \forall v$$

↑ Hodge star

$$\text{vol}(\omega, u, v) = Wu \cdot v$$

Power as a linear functional on velocity fields

Force

$\mathcal{F}(v)$ representation

special form

$$\mathcal{F}(v) = f_A \cdot v(p_A) + f_B \cdot v(p_B) + f_C \cdot v(p_C)$$

more general

$$\mathcal{F}(v) = \int_{\mathcal{R}} b(x) \cdot v(x) dV + \int_{\partial \mathcal{R}} t(x) \cdot v(x) d\Delta$$

velocity field

$$r(c(t)) = r(c(0)) + \nabla r(c(0)) (r(c(t)) - r(c(0))) + o(t)$$

$$r(x) = r_0 + \nabla r (x - p_0) \quad \text{affine}$$

$$\nabla r = \dot{R} R^T = W \quad \text{rigid}$$

$$\begin{aligned} W u_A \cdot f_A &= \omega \times u_A \cdot f_A \\ &= f_A \cdot \omega \times (p_A - p_0) = (p_A - p_0) \times f_A \cdot \omega \end{aligned}$$

$$\begin{aligned} \mathcal{F}(V) &= f_A \cdot r(p_A) + f_B \cdot r(p_B) + f_C \cdot r(p_C) \\ &= f_A \cdot r_0 + f_A \cdot \omega \times (p_A - p_0) + \dots \\ &= f_A \cdot r_0 + (p_A - p_0) \times f_A \cdot \omega + \dots \\ &= \dots = f \cdot r_0 + m \cdot \omega \end{aligned}$$

$$\mathcal{F}(V) = \int_{\mathcal{R}} b(x) \cdot r(x) dV + \int_{\partial \mathcal{R}} t(x) \cdot r(x) dA$$

Bulk force
(density with respect
to the volume)

per unit volume

Traction
(density with respect
to the area)

per unit area

$$\begin{aligned} &= \left(\int_{\mathcal{R}} b(x) dV + \int_{\partial \mathcal{R}} t(x) dA \right) \cdot r_0 \\ &+ \left(\int_{\mathcal{R}} (x - p_0) \times b(x) dV + \int_{\partial \mathcal{R}} (x - p_0) \times t(x) dA \right) \cdot \omega \\ &= f \cdot r_0 + m \cdot \omega \end{aligned}$$

(27-28)₅

Tuesday [2014-03-25]

example 1

$$t(x) = 0, \quad b(x) = \rho g \quad g \text{ is a vector}$$

$$f = \int_{\mathcal{R}} \rho g \, dV = \rho g \, \text{Vol}(\mathcal{R}) = \underbrace{\rho \, \text{Vol}(\mathcal{R})}_{\text{total mass}} g$$

$$m = \int_{\mathcal{R}} (x - p_0) \times (\rho g) \, dV = \int_{\mathcal{R}} (x - p_0) \, dV \times (\rho g)$$

$$\frac{1}{V} \int_{\mathcal{R}} (x - p_0) \, dV = (x_G - p_0)$$

↑ barycenter of \mathcal{R}

if $p_0 = x_G$ then $m = 0$

example 2

$$b(x) = 0, \quad t(x) = \rho g \quad \rho \text{ "skin" mass density}$$

$$f = \int_{\partial\mathcal{R}} \rho g \, dA = \rho \, \text{Area}(\partial\mathcal{R}) g; \quad m = \int_{\partial\mathcal{R}} (x - p_0) \, dA \times (\rho g)$$

$$\frac{1}{A} \int_{\partial\mathcal{R}} (x - p_0) \, dA = (x_G - p_0)$$

↑ barycenter of $\partial\mathcal{R}$

Balance principle

$$\mathcal{F}(v) = 0 \quad \forall v$$

$$v(x) = v_0 + W(x - p_0)$$

$$\Rightarrow \mathcal{F}(v) = f \cdot v_0 + m \cdot \omega$$

$$\mathcal{F}(v) = 0 \quad \forall v \Leftrightarrow f = 0, m = 0$$

v general continuous and differentiable vector field

$$\mathcal{F}(v) = \int_{\mathcal{R}} b(x) \cdot v(x) dV + \int_{\partial \mathcal{R}} t(x) \cdot v(x) dV$$

$$\mathcal{F}(v) = 0 \quad \forall v \Rightarrow b = 0, t = 0 \quad \text{no force is allowed}$$

A convenient approach consists in setting

$$\mathcal{F}(v) = \mathcal{F}^{ext}(v) + \mathcal{F}^{int}(v)$$

based on a suitable characterization of the two different parts, and still requiring

$$\mathcal{F}(v) = 0 \quad \forall v$$

In order to have some insight into the way of characterizing the force distribution let us consider just the extension of rigid velocity fields to affine velocity fields:

$$v(x) = v_0 + L(x - p_0)$$

where L is the velocity gradient (a tensor)

$$f^{\text{ext}}(v) = f_A \cdot v_A + f_B \cdot v_B + f_C \cdot v_C$$

$$= f_A \cdot v_0 + f_A \cdot L(p_A - p_0) + \dots$$

$$= f_A \cdot v_0 + (p_A - p_0) \otimes f_A \cdot L + \dots$$

$$= (f_A + f_B + f_C) \cdot v_0$$

$$+ ((p_A - p_0) \otimes f_A + (p_B - p_0) \otimes f_B + (p_C - p_0) \otimes f_C) \cdot L$$

$$= f \cdot v_0 + M \cdot L$$

(29-30)₅ Wednesday [2014-03-26]

$$f_A \cdot L (P_A - P_0) = (P_A - P_0) \otimes f_A \cdot L \quad \otimes, \otimes \quad \begin{array}{l} \text{Gurtin} \\ \downarrow \end{array}$$

$$M \cdot L = \text{tr}(M^T L) = f_A \otimes (P_A - P_0)$$

$$\text{tr}(AB) = \frac{\text{vol}(ABe_1, e_2, e_3) + \dots}{\text{vol}(e_1, e_2, e_3)}$$

$$Be_i = b_{1i}e_1 + b_{2i}e_2 + b_{3i}e_3$$

$$Ae_i = a_{1i}e_1 + a_{2i}e_2 + a_{3i}e_3$$

any basis

$$ABe_i = b_{1i}Ae_1 + b_{2i}Ae_2 + b_{3i}Ae_3$$

$$= b_{1i}(a_{11}e_1 + a_{21}e_2 + a_{31}e_3)$$

$$+ b_{2i}(a_{12}e_1 + a_{22}e_2 + a_{32}e_3)$$

$$+ b_{3i}(a_{13}e_1 + a_{23}e_2 + a_{33}e_3)$$

$$\text{vol}(ABe_1, e_2, e_3) = (b_{11}a_{11} + b_{21}a_{12} + b_{31}a_{13})$$

$$\text{vol}(e_1, ABe_2, e_3) = (b_{12}a_{21} + b_{22}a_{22} + b_{32}a_{23})$$

$$\text{vol}(e_1, e_2, ABe_3) = (b_{13}a_{31} + b_{23}a_{32} + b_{33}a_{33})$$

If we exchange A and B the sum above will be left unchanged. So $\text{tr}(AB) = \text{tr}(BA)$

$$M \cdot L = \text{tr}(M^T L)$$

$$\text{tr}(M^T L) = m_{11}^T v_{11} + m_{21}^T v_{12} + m_{31}^T v_{13}$$

+

+

By using an orthonormal basis we realize that

since $m_{21}^T = m_{12}$ then

$$\text{tr}(M^T L) = \sum \sum m_{ij} v_{ij}$$

$$A \cdot W = \text{tr}(A^T W) = \text{tr}(W^T A) = W \cdot A$$

$$\left. \begin{array}{l} A^T = A \\ W^T = -W \end{array} \right\} \Rightarrow = \text{tr}(AW) = -\text{tr}(WA) = -\text{tr}(AW)$$

$$\Rightarrow A \cdot W = 0$$

Properties of "tr"

$$\text{tr}(A) = \text{tr}(A^T)$$

$$\text{tr}(AB) = \text{tr}(BA)$$

$$\begin{aligned}
 M \cdot L &= (\text{skw } M + \text{sym } M) \cdot (W + D) \\
 &= \text{skw } M \cdot W + \cancel{\text{skw } M \cdot D} \\
 &\quad + \cancel{\text{sym } M \cdot W} + \text{sym } M \cdot D
 \end{aligned}$$

$$\begin{aligned}
 \mathbb{F}^{\text{ext}}(r) &= f \cdot r_0 + M \cdot L \\
 &= f \cdot r_0 + \text{skw } M \cdot W + \text{sym } M \cdot D
 \end{aligned}$$

r affine velocity field

$$r(x) = r_0 + L(x - p_0)$$

r rigid velocity field ($L = W$)

$$\mathbb{F}^{\text{ext}}(r) = f \cdot r_0 + \underbrace{\text{skw } M \cdot W}_{m \cdot \omega}$$